REPORT ON REPORT OF SLABS REINFORCED
WITH HIGH-STRENGTH STARK STEEL RE BARS
PHASE-3 WITH HIGH-STRENGTH STARK STEEL RE BARS

PHASE-3

Investigator

Dr. S. Suriya Prakash Professor Department of Civil Engineering IIT-Hyderabad Kandi, Sangareddy District 502285

Date Submitted

09/05/2023

Disclaimer

This report summarizes the test results of slabs reinforced with STARK steel rebar subjected to punching shear load.

Dr. S. SURIYA PRAKASH
Professor and Head
Department of Civil Engineering
Indian Institute of Technology Hyderabad
Kana-502285, Sangareday, Telangana, India

Contents

List of Tables

List of Figures

1.INTRODUCTION

This study explores the performance of the use of high-strength steel rebars for on-grade slab applications. The load-carrying capacity of square slabs of size 1 m x 1m reinforced with high-strength **1. INTRODUCTION**
This study explores the performance of the use of high-strength steel rebars for on-grade slab
applications. The load-carrying capacity of square slabs of size 1 m x 1m reinforced with high-strength
Stark **1. INTRODUCTION**

This study explores the performance of the use of high-strength steel rebars for on-grade slab

applications. The load-carrying capacity of square slabs of size 1 m x 1 m reinforced with high-strength

S spacing of rebars were considered as test parameters. **TRODUCTION**
This study explores the performance of the use of high-strength steel rebars for on-grade slab
rations. The load-carrying capacity of square slabs of size 1 m x 1m reinforced with high-strength
steel rebars u **1. INTRODUCTION**

This study explores the performance of the use of high-strength steel rebars for on-grade slab

applications. The load-carrying capacity of square slabs of size 1 m x 1 m reinforced with high-strength

S

2.EXPERIMENTAL PROGRAM

are the spacing of reinforcement and the depth of the slab. Two types of spacing were considered (150

Designation of Specimen	Depth (D) (mm)	Spacing (S) (mm)	Length (L) (mm)	Amount of reinforcement (kg/m ²)
P D170 S150 S1	170	150	1000	2.30
P D170 S150 S2	170	150	1000	2.30
P D170 S200 S1	170	200	1000	1.65
P D170 S200 S2	170	200	1000	1.65
P D150 S150 S1	150	150	1000	2.30
P D150 S150 S2	150	150	1000	2.30
P D150 S200 S1	150	200	1000	1.65
P D150 S200 S2	150	200	1000	1.65

Table 1:Details of test specimens

2.1. Materials and mix proportions

The concrete mix of grade M25 was designed using IS 10262 and IS 456 code recommendations. Ordinary Portland cement (OPC) of 53 grade conforming to IS 4031-1988 was used to develop the design concrete mix. The specific gravity of cement was 3.15. Locally available natural sand was used as fine aggregate. The fine aggregate corresponded to Zone-III grading requirement of IS 383-1970. The specific gravity of fine aggregate was 2.7 and its fineness modulus was 2.2. The locally available crushed granite rock with a specific gravity of 2.79 was used as coarse aggregate and a nominal size of 10 mm. The mix proportion of cement, **F** D170 S200 S2 170 200 1000 1.65
 P D150 S150 S1 150 150 1000 2.3.0
 P D150 S150 S2 150 160 1000 1.65
 P D150 S200 S1 150 200 1000 1.65
 P D150 S200 S1 150 200 1000 1.65
 P D150 S200 S1 150 200 1000 1.65
 Not ratio of 0.55 was used throughout the entire mix. High-strength Stark steel rebars with yield strength of 1700 MPa was adopted. The mechanical properties of the steel rebars used are given in Table 2.

Table 2:Mechanical properties of steel rebars

-
-
-
-

Slabs of length 1000 mm and breadth 1000 mm of varying depths were cast with two different

Reinforced with Stark steel @ 150mm c/c $cc=25$ mm $cc=25$ mm

Bar length=950mm Bar length=950mm $e=25$ mm $e=75$ mm $c=25$ mm $c=25$ mm Reinforced with Stark steel @ 200 mm c/c

Reinforced with Stark steel ω 150mm c/c Bar length=950mm $e=25$ mm c=25 mm cc=25 mm

Reinforced with Stark steel @ 200 mm c/c Bar length=950mm $e=75$ mm $c=25$ mm cc=25 mm

The wooden moulds were prepared for specimens to be cast, as shown in Figure 3b. The wooden with Stark steel (@ 150mm c/c Bar length-950mm and $e-25$ mm $e-25$ m E

succross A can be a control of the sum of the sum of the set of $\frac{1}{2}$ can be a control of the set of $\frac{1}{2}$ can be a capital space of the spacing matrix of $\frac{1}{2}$ can be a capital space of $\frac{1}{2}$ can be a spectros A-A

e free length; c-edge distance, co-clear cover

Reinforced with Stark steel @ 150mm c/c

Bar length-950mm

e-25 mm

e-25 mm

c-25 mm

c sections AA
 e free length; c=edge distance, cc=dear cover

Reinforced with Stark steel (@ 150mm c/c

Bar length=950mm
 e =25 mm
 e -25 mm
 e -25 mm
 e -25 mm
 e -25 mm

Tigure 2: Reinforcement detailing for square e= free length; c=edge distance, cc=clear cover

Reinforced with Stark steel @ 200 mm c/c

Bar length=950mm

e=25 mm

c=25 mm

c=25 mm

c=25 mm

c=25 mm

Figure 2: Reinforcement detailing for square slab of 170mm depth

2 Reinforced with Stark steel @ 150mm c/c

Bar lcngth=950mm

Bar lcngth=950mm

e=25 mm

e=25 mm

cc=25 mm

cc=25 mm

cc=25 mm

cc=25 mm

cc=25 mm

cc=25 mm

ec=25 mm

Figure 2: Reinforcement detailing for square stab of 170 Reinforced with Stark steel @ 150mm c/c

Bar length-950mm

Bar length-950mm
 $c=25$ mm
 $c=25$ mm
 $c=25$ mm
 $c=25$ mm

Eigure 2: Reinforcement detailing for square stab of 170mm depth

2.2. Specimen Preparation

Tigure $c=25$ mm
 $c=25$ mm
 $c=25$ mm
 $c=-25$ mm

Figure 2: Reinforcement detailing for square slab of 170mm depth

men Preparation

wooden moulds were prepared for specimens to be cast, as shown in Figure 3b. The

g mats with cc=25 mm

Figure 2: Reinforcement detailing for square slab of 170mm depth

Specimen Preparation

The wooden moulds were prepared for specimens to be cast, as shown in Figure 3b. The

orcing mats with two different spacin Figure 2: Reinforcement detailing for square slab of 170mm depth

Specimen Preparation

The wooden moulds were prepared for specimens to be cast, as shown in Figure 3b. The

Toring mats with two different specings were pl

Figure 3: a) Slump test b) Wooden mould

2.3. Testing of specimens

The specimens were tested using servo-controlled actuator of 1000 kN capacity using digital closed-loop control. The test set-up of the specimen and instrumentation used are shown in Figure 4. The mid-span displacement was measured using a linear variable differential transducer (LVDT). Strain variation in the reinforcement bar has been measured from the strain gauges attached to the rebars. The Load, displacement, and time results are simultaneously acquired through a data acquisition system.

Figure 4: Punching shear test set-up

3. RESULTS AND DISCUSSIONS FROM MECHANICAL TESTING
The experimental data such as Load vs mid-span displacement and strain values
acquired during the tests are analyzed. The Load vs displacement behavior and the crack
patte ULTS AND DISCUSSIONS FROM MECHANICAL TESTING
The experimental data such as Load vs mid-span displacement and strain values
ed during the tests are analyzed. The Load vs displacement behavior and the crack
are shown in the **EXECULTS AND DISCUSSIONS FROM MECHANICAL TESTING**
The experimental data such as Load vs mid-span displacement and strain values
acquired during the tests are analyzed. The Load vs displacement behavior and the crack
patte **RESULTS AND DISCUSSIONS FROM MECHANICAL TESTING**
The experimental data such as Load vs mid-span displacement and
acquired during the tests are analyzed. The Load vs displacement behavior a
pattern are shown in the followi **NS FROM MECHANICAL TESTING**

as Load vs mid-span displacement and strain values

strated. The Load vs displacement behavior and the crack

figures.
 3.1 Punching shear test

P_D170_S150
 $-\frac{p_{.D170_S150_S1}}{p_{.D170_S150_S2}}$

10 20 30 40 50 60 70 80

Deflection (mm)

eflection response of the specimen D170_S150 under punching loading

Table 4:Average values for D170_S150 in tonnes

rable 4 250 $\frac{200}{25}$
 $\frac{25}{25}$
 $\frac{150}{25}$
 $\frac{150}{25}$
 $\frac{50}{25}$
 $\frac{150}{25}$

SPECIMEN: P_D170_S150

	\tilde{S} 100 50 $\bf{0}$ $\bf{0}$	10	20	30 40 Deflection (mm) Figure 5: Load vs Deflection response of the specimen D170_S150 under punching loading Table 4: Average values for D170_S150 in tonnes	50 60	P_D170_S150_S1 P_D170_S150_S2 70 80	
S. No		Sample ID		Cracking Load (tonnes)	Average Cracking Load (tonnes)	Ultimate Load (tonnes)	Average Ultimate Load (tonnes)
1.		D170_S150_S1		11.52		20.12	
2.		D170_S150_S2		9.24	10.37	20.28	20.20

Figure 6:Failure mode of the specimen D170_S150

SPECIMEN: P_D170_S200

Figure 8: Failure mode of the specimen D170_S200

SPECIMEN: P_D150_S150

	$\overline{5}$ $\bf{0}$	15 10 Deflection (mm)	20	25	30
	Figure 9: Load vs Deflection response of the specimen D150_S150 under punching loading				
		Table 6: Average values for D150_S150 in tonnes			
S. $\mathbf{N}\mathbf{0}$	Sample ID	Cracking Load (tonnes)	Average Cracking Load (tonnes)	Ultimate Load (tonnes)	Average Ultimate Load (tonnes)
1.	D150_S150_S1	8.34	8.45	18.13	18.15

Table 6:Average values for D150_S150 in tonnes

Figure 10: Failure mode of the specimen D150_S150

SPECIMEN: P_D150_S200

Figure 11: Load vs Deflection response of the specimen D150_S200 under punching loading

	М 50				
	$\bf{0}$ 10 $\bf{0}$	20 30	40 50 Deflection (mm)	${\bf 70}$ 60	80
		Figure 11: Load vs Deflection response of the specimen D150_S200 under punching loading Table 7: Average values for D150_S200 in tonnes			
S. No	Sample ID	Cracking Load (tonnes)	Average Cracking Load (tonnes)	Ultimate Load (tonnes)	Average Ultimate Load (tonnes)
1.	D150_S200_S1	6.23		11.86	11.96
2.	D150_S200_S2	7.03	6.63	12.06	

Table 7:Average values for D150_S200 in tonnes

Figure 12:Failure mode of the specimen D150_S200

OBSERVATIONS:

- Stark Steel demonstrated satisfactory ductility performance and commendable loadcarrying capacity under punching loading, without any strand rupture observed until the ultimate load.
- The steel's elongation of 5.4%, measured from a previous tensile test, suggests its good formability and ability to deform before breaking.
- Based on the experimental results, Stark Steel is suitable for applications requiring high strength and resistance to mechanical stress.
- **THE OREST CONSET SET AS A SET ASSEM STATE OF STATE STATE OF STATE AND SET SET AND A SURPRESS CRACK PROPERTIES** alternate load The steel's elongation of 5.4%, measured from a previous tensile test, suggests its good formab a high level of indeterminacy, making it advantageous for applications where structural redundancy is essential for safety and reliability.

4. SUMMARY

• The study investigated the performance of slabs reinforced with high-strength Stark steel rebars under punching loading. Slabs of two different depths with different spacing were considered. SERVATIONS:

STRAT Steel demonstrated satisfactory ductility performance and commendable load-

carrying eapacity under punching loading, without any strand rupture observed until the

ultimate load.

In steels clongation earry and a distinguishing conding, without any strand rupture observed until the

ultimate load.

The steel's clongation of 5.4%, measured from a previous tensile test, suggests its good

formability of deform before brea The steels elongation of 5.4%, measured from a previous tensile test, suggests its good
formability and ability to deform before breaking.
Based on the experimental results, Stark Steel is suitable for applications requiri formability to deform before breaking.

Based on the experimental results. Stark Steel is suitable for applications requiring high

sterpgth and resistance to mechanical stress.

The observed crack pattern in the specience iased on the experimental results, Stark Steel is suitable for applications requiring high
renepth and resistance to mechanical stress.
The observed crack pattern in the specimens indicates that the slab of Stark Steel exh

REFERENCES

- Concrete, Bureau of Indian Standards, New Delhi.
- Standards, New Delhi.
-
-

